



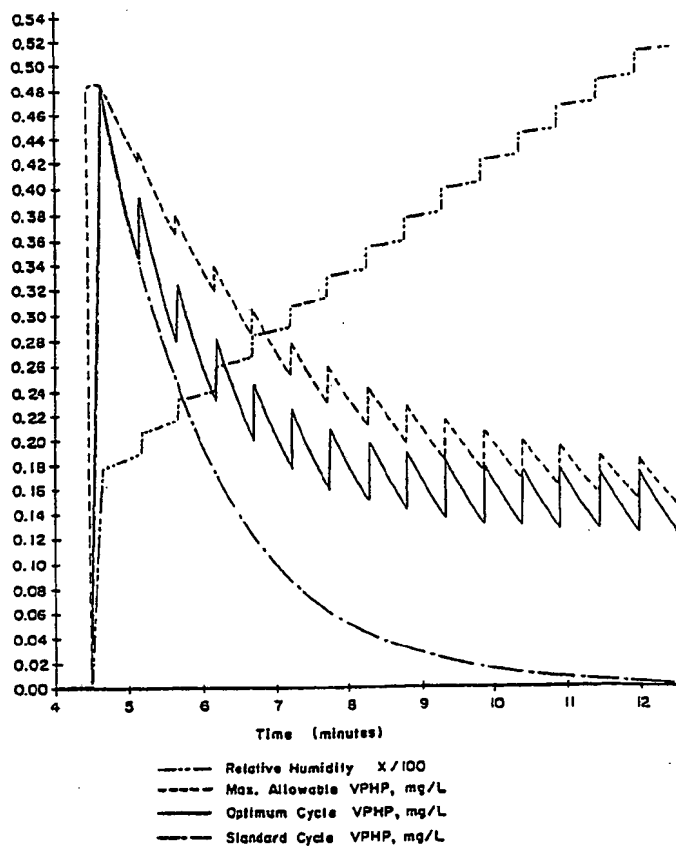
## INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

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## (54) Title: OPTIMUM HYDROGEN PEROXIDE VAPOR STERILIZATION METHOD

## (57) Abstract

A sterilization method including the steps of injecting a hydrogen peroxide and water vapor mixture into a closed sterilization chamber of a predetermined volume at a predetermined temperature in an initial amount up to the saturation limit of such vapor mixture and thereafter, injecting a plurality of intermittent make-up injections of such vapor mixture into the chamber. The rate of the make-up injections and the amount of each such make-up injection is based on the rate and amounts necessary to maintain the concentration of hydrogen peroxide vapor at a level effective for sterilization but less than that which would raise the concentration of the vapor mixture to the saturation limit which will be present in the chamber immediately following injection of a make-up injection.



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## OPTIMUM HYDROGEN PEROXIDE VAPOR STERILIZATION METHOD

BACKGROUND OF THE INVENTIONField of the Invention

The present invention relates to methods of sterilization, and more particularly, to a method of vapor phase hydrogen peroxide sterilization.

Description of the Prior Art

In 1979 Moore et al. disclosed in U.S. Patent No. 4,169,123 a method of sterilizing with "cold" hydrogen peroxide vapor. Forstrom et al. disclosed a similar method wherein the concentration of the hydrogen peroxide vapor is less than 75 mg/L. Bier U.S. Patent No. 4,642,165 discloses a method of vaporizing multicomponent liquids such as hydrogen peroxide and water, and passing the vapor in successive small increments into a sterilization chamber.

Hydrogen peroxide is rarely, if ever, used in a pure form. It is typically mixed with water. Hydrogen peroxide vapor, like water vapor, is a condensable gas, but is less volatile than water vapor. When injected into a sterilizer with water vapor, the hydrogen peroxide vapor may readily decompose into water and oxygen or condense into liquid. Thus, the concentration of vapor phase hydrogen peroxide within a sterilization chamber will decrease with time as degradation and/or condensation occurs.

It is necessary in order to achieve effective sterilization, to maintain the concentration of the sterilant at effective levels throughout the sterilization phase of a cycle. The Bier patent referenced above discloses that the multicomponent vapor should be introduced in successive increments but it does not address the question of the

degradation of the hydrogen peroxide vapor after injection into the sterilization chamber or the problems of exceeding the saturation limit of the vapor mixture.

- 5        One problem with indiscriminate successive injections of a hydrogen peroxide and water vapor mixture into the sterilization chamber is that the concentrations of the condensable vapors can exceed the saturation limit of the mixture causing the vapors to condense. The saturation limit generally increases with increasing temperature and varies with the relative concentrations of the different molecular species of the mixture. When the mixture is comprised of hydrogen peroxide and water the problem is
- 10        compounded because of the degradation of hydrogen peroxide into water and oxygen. The increase in water vapor concentration resulting from such degradation reduces the saturation limit of the mixture and accordingly, reduces the maximum hydrogen peroxide.
- 15        vapor concentration that can be injected into the chamber without causing the vapor mixture to condense.

It is an object of the present invention to provide a vapor phase hydrogen peroxide sterilization method wherein the problems of exceeding the saturation limit of the vapor mixture and the degradation of hydrogen peroxide vapor to water vapor and oxygen are overcome. It is a further object of the present invention to provide an optimum vapor phase hydrogen peroxide sterilization method in order

25        to ensure that an effective level of hydrogen peroxide

30        is maintained in the sterilization chamber.

SUMMARY OF THE INVENTION

The present invention provides an optimum hydrogen peroxide vapor sterilization method. The method succeeds in maintaining an effective level of hydrogen peroxide vapor in the sterilization chamber to ensure effective sterilization. The method includes the steps of injecting a hydrogen peroxide and water vapor mixture into a sterilization chamber having a predetermined volume at a predetermined temperature in an initial amount less than the saturation limit of the vapor mixture in the chamber at such temperature and such volume and thereafter, injecting a plurality of intermittent make-up injections of the vapor mixture into the chamber, the make-up injections being at a rate and each such make-up injection being in a variable amount necessary to maintain the concentration of hydrogen peroxide vapor at a level effective for sterilization but less than that concentration of hydrogen peroxide vapor which would raise the concentration of the vapor mixture to the saturation limit which will be present in the chamber immediately following injection of such make-up injection at such temperature.

The hydrogen peroxide and water vapor mixture is preferably a 30% by weight composition at about 4°C. The saturation limits and the initial and variable amounts of the vapor mixture may be determined by continuously monitoring the hydrogen peroxide vapor concentration and the water vapor concentration within the chamber. Alternatively, the saturation limits and the initial and variable amounts of the vapor mixture may be predetermined according to the procedures set forth in more detail hereinbelow.

BRIEF DESCRIPTION OF THE FIGURES

The present invention can be better understood by reference to the figures in which:

FIG. 1 is a graph showing a preferred embodiment  
5 of the optimum hydrogen peroxide vapor sterilization method of the present invention wherein a 30 wt% hydrogen peroxide and water vapor mixture is injected into an evacuated sterilization chamber and followed by a plurality of make-up injections;

10 FIG. 2 is a graph showing the hydrogen peroxide vapor concentration over time based on the sterilization cycle of FIG. 1;

FIG. 3 is a graph showing the water vapor concentration over time based on the sterilization  
15 cycle of FIG. 1;

FIG. 4 is a graph comparing relative humidity, maximum allowable hydrogen peroxide vapor concentration, the standard hydrogen peroxide vapor concentration over time obtained from a single  
20 injection of vapor and the optimum hydrogen peroxide vapor concentration over time based on the preferred embodiment of the sterilization method of the present invention;

FIG. 5 is a graph showing the projected decrease  
25 in the degree of saturation of the vapor mixture in the simulation of a hydrogen peroxide sterilization cycle wherein a 30 wt% hydrogen peroxide and water vapor mixture is injected in a single injection into an evacuated sterilization chamber and held for a time  
30 with no make-up injections;

FIG. 6 is a graph showing the projected decrease in hydrogen peroxide concentration over time based on the sterilization cycle of FIG. 5;

FIG. 7 is a graph showing the projected rise in water vapor concentration over time based on the sterilization cycle of FIG. 5;

FIG. 8 is a graph showing the elevated degree of saturation of the vapor mixture in a sterilization cycle which incrementally compensates for lost hydrogen peroxide vapor by injecting a 30 wt% hydrogen peroxide and water vapor mixture in amounts equal to the amount of hydrogen peroxide vapor decomposed;

FIG. 9 is a graph showing the hydrogen peroxide vapor concentration over time based on the sterilization cycle of FIG. 8;

FIG. 10 is a graph showing the water vapor concentration over time based on the sterilization cycle of FIG. 8; and

FIG. 11 is a graph showing the degree of condensation over time based on the sterilization cycle of FIG. 8.

#### DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

The optimum hydrogen peroxide vapor sterilization cycle of the present invention is illustrated graphically in FIGS. 1 through 4. For comparison, and to illustrate the advantages of the optimum sterilization cycle of the present invention, the consequences of two other hydrogen peroxide vapor sterilization cycles are illustrated in FIGS. 5 through 11.

To illustrate the problem of hydrogen peroxide degradation, refer to FIGS. 5 through 7, which simulate the activity within an evacuated 49.29 L sterilization chamber at 4°C when there is a single injection of 30 wt% hydrogen peroxide-water vapor.

In FIG. 5, the scale of the vertical axis runs from zero to 100. For the solid line this means zero

to 100 mm Hg (torr) pressure. Thus, atmospheric pressure (760 torr) is off scale. As the cycle starts (time=0) air is withdrawn from the chamber and the pressure decreased from 760 torr to about 2 torr. At 5 time=4.5 minutes, a mixture of hydrogen peroxide and water vapors is injected into the chamber causing a small rise in pressure. The pressure thereafter appears nearly constant (the "hold period"), until 10 time=11.2 minutes, when air is allowed into the chamber ("air break"), causing an abrupt rise in pressure to 50 torr. The chamber is again evacuated, followed by air to 50 torr, evacuation, and air to atmospheric.

The dashed line in FIG. 5 illustrates the degree 15 of saturation of the hydrogen peroxide and water vapor mixture in the chamber. It peaks to 100% upon injection of vapors (time=4.5), as planned. Immediately, however, it drops, as hydrogen peroxide vapors decompose.

20 FIG. 6 shows hydrogen peroxide vapor concentration during this cycle. The concentration drops nearly to zero during the hold period. This is undesirable because sterilization requires the maintenance of an effective level of hydrogen peroxide 25 vapor throughout the entire sterilization hold period.

FIG. 7 shows that water vapor concentration rises during the sterilization hold period as hydrogen peroxide decomposition produces water vapor (and oxygen).

30 One might expect that a reasonable way to counteract the decrease in hydrogen peroxide vapor concentration during the sterilization hold period would be to inject more hydrogen peroxide to replace the amount lost.



FIG. 8 illustrates a cycle which incrementally compensates for lost hydrogen peroxide vapor by injecting 30 wt% hydrogen peroxide-water vapor. The amount of hydrogen peroxide vapor injected equals the amount of hydrogen peroxide vapor decomposed since the last injection. The pressure trace reflects the small pressure rises with each increment. The vapor saturation trace shows that each injection reaches saturation.

FIG. 9 depicts the hydrogen peroxide vapor concentration associated with FIG. 8. Hydrogen peroxide vapor decreases almost as fast as it did without compensating injections. This is because water vapor concentration increases rapidly (See FIG. 10), due partly to decomposition of hydrogen peroxide vapor, but mostly from water vapor accompanying the hydrogen peroxide vapor in the compensating injections. As a result, the saturation limit decreases. The compensating injections exceed the saturation limit, causing condensation of hydrogen peroxide and some water. FIG. 11 shows the amount of condensate increasing from zero to 2.1 mg/L (105 mg condensate / 49.29 L chamber volume) because of the compensating injections.

The optimum hydrogen peroxide vapor sterilization method of the present invention overcomes the problems of hydrogen peroxide vapor degradation and condensation by employing knowledge concerning the changing saturation limit of hydrogen peroxide vapor during the sterilization cycle, particularly during the sterilization hold period, and introducing intermittent make-up injections of the hydrogen peroxide-water vapor mixture wherein the amount of each make-up injection maintains the hydrogen peroxide

sterilization but less than that which would raise the concentration of the vapor mixture to the saturation limit which will be present in the chamber immediately following such make-up injection at that point during the sterilization hold period.

FIG. 1 illustrates the improved approach to the dilemma under the same conditions as those represented in FIGS. 5 and 8. As FIG. 2 illustrates, the hydrogen peroxide vapor concentration does not decrease as rapidly as it would in the other approaches represented in FIGS. 6 and 9. FIG. 3 illustrates the rise in water vapor concentration during the sterilization hold period of the sterilization cycle of the present invention.

The optimum hydrogen peroxide vapor sterilization method can be practiced in a vacuum chamber, as illustrated in the Figures, or in a static chamber. The method is not pressure dependent. In addition, the sterilization system would require a source of the desired hydrogen peroxide and water mixture, a vaporizer and valves capable of delivering precisely measured variable amounts of the hydrogen peroxide-water mixture to the vaporizer and then into the chamber. Because the timing and amounts of the vapor mixture to be delivered to the chamber are so important, a suitably programmed computer for controlling the injections is also desirable.

The purpose of the method is to maximize hydrogen peroxide vapor exposure during the cycle. Maximum exposure can result in reduced cycle time and/or greater assurance of sterilization. The sterilization cycle shown in FIG. 1 includes the steps of evacuating a sterilization chamber of a predetermined volume, injecting a hydrogen peroxide-water vapor mixture of a desired percent composition into the sterilization

chamber at a desired temperature in an amount up to the amount necessary to reach the saturation limit of the vapor mixture associated with the volume of the chamber, the temperature and the concentration of the vapor mixture, and injecting a plurality of intermittent make-up injections of the vapor mixture at a rate based on the rate of degradation of hydrogen peroxide vapor within the chamber. The amount of the vapor mixture in each such make-up injection is preferably just below the hydrogen peroxide concentration which would reach the saturation limit of the vapor mixture which will be present in the chamber immediately following each such make-up injection. The make-up injections are continued through the sterilization hold period of the cycle to maintain an optimum level of hydrogen peroxide vapor within the chamber necessary for effective sterilization without inducing appreciable condensation.

Following the sterilization hold period, the vapor mixture is exhausted from the chamber. The chamber is then aerated and again exhausted to ensure the complete removal of all of the sterilant vapor mixture. The aeration and evacuation steps may be repeated before the chamber is returned to atmospheric pressure.

FIGS. 1-3 were constructed based on the sterilization cycle data set forth in Table I below.

TABLE I

H<sub>2</sub>O<sub>2</sub> CYCLE  
IN 49.29 L CHAMBER AT 4°C

5	step	TIME min.	H <sub>2</sub> O <sub>2</sub> mg/L	H <sub>2</sub> O <sub>2</sub> satn mg/L	Water mg/L	RH %	VAPOR % satn	P torr	AMOUNT INJCTD
	Close Door	0.00	0.000		1.94	30.00		760.0	0.0
	vacuum/start	0.45	0.000	0.00	1.00	15.45	15.5	391.5	0.0
	vacuum/mid	2.25	0.000	0.00	0.07	1.09	1.1	27.6	0.0
10	vacuum/end	4.50	0.000	0.00	0.00	0.04	0.0	1.0	0.0
	inject/start	4.50	0.049	0.48	0.12	1.80	10.1	1.1	8.0
	inject/mid	4.60	0.243	0.49	0.57	8.84	50.1	1.7	40.0
	inject/end	4.70	0.486	0.49	1.14	17.64	100.0	2.3	80.0
	hold/start	4.78	0.459	0.47	1.15	17.86	96.6	2.3	80.0
15	hold/end	5.20	0.344	0.42	1.21	18.81	81.8	2.3	80.0
	inject	5.20	0.392	0.43	1.33	20.57	91.8	2.5	88.0
	hold/start	5.30	0.370	0.42	1.34	20.75	88.9	2.5	88.0
	hold/end	5.70	0.277	0.36	1.39	21.51	76.2	2.5	88.0
	inject	5.70	0.326	0.38	1.50	23.27	86.4	2.6	96.0
20	hold/start	5.80	0.308	0.37	1.51	23.42	83.8	2.6	96.0
	hold/end	6.22	0.231	0.32	1.55	24.05	72.5	2.6	96.0
	inject	6.22	0.279	0.34	1.67	25.81	82.9	2.7	104.0
	hold/start	6.32	0.264	0.33	1.67	25.94	80.6	2.7	104.0
	hold/end	6.74	0.197	0.28	1.71	26.49	70.4	2.7	104.0
25	inject	6.74	0.246	0.30	1.82	28.25	81.1	2.9	112.0
	hold/start	6.84	0.232	0.29	1.83	28.36	78.9	2.9	112.0
	hold/end	7.26	0.174	0.25	1.86	28.84	69.4	2.9	112.0
	inject	7.26	0.223	0.28	1.97	30.60	80.4	3.0	120.0
	hold/start	7.36	0.210	0.27	1.98	30.70	78.3	3.0	120.0
30	hold/end	7.78	0.157	0.23	2.01	31.13	69.4	3.0	120.0
	inject	7.78	0.206	0.26	2.12	32.89	80.6	3.1	128.0
	hold/start	7.88	0.195	0.25	2.13	32.99	78.6	3.1	128.0
	hold/end	8.30	0.146	0.21	2.15	33.39	70.0	3.1	128.0
	inject	8.30	0.194	0.24	2.27	35.15	81.4	3.3	136.0
35	hold/start	8.40	0.184	0.23	2.27	35.24	79.5	3.3	136.0
	hold/end	8.82	0.138	0.19	2.30	35.62	71.1	3.3	136.0
	inject	8.82	0.186	0.23	2.41	37.38	82.7	3.4	144.0
	hold/start	8.92	0.176	0.22	2.42	37.46	80.9	3.4	144.0
	hold/end	9.34	0.132	0.18	2.44	37.82	72.6	3.4	144.0
40	inject	9.34	0.180	0.21	2.55	39.58	84.4	3.5	152.0
	hold/start	9.44	0.170	0.21	2.56	39.67	82.5	3.5	152.0
	hold/end	9.86	0.128	0.17	2.58	40.02	74.3	3.5	152.0
	inject	9.86	0.176	0.20	2.70	41.78	86.3	3.7	160.0
	hold/start	9.96	0.166	0.20	2.70	41.86	84.5	3.7	160.0
45	hold/end	10.38	0.125	0.16	2.72	42.20	76.2	3.7	160.0
	inject	10.38	0.173	0.20	2.84	43.96	88.4	3.8	168.0

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	hold/start	10.48	0.164	0.19	2.84	44.04	86.6	3.8	168.0
	hold/end	10.90	0.123	0.16	2.86	44.38	78.3	3.8	168.0
	inject	10.90	0.171	0.19	2.98	46.14	90.7	3.9	176.0
	hold/start	11.00	0.162	0.18	2.98	46.22	88.8	3.9	176.0
5	hold/end	11.42	0.121	0.15	3.00	46.55	80.5	3.9	176.0
	inject	11.42	0.170	0.18	3.12	48.31	93.0	4.1	184.0
	hold/start	11.52	0.160	0.18	3.12	48.39	91.1	4.1	184.0
	hold/end	11.94	0.120	0.14	3.14	48.72	82.8	4.1	184.0
	inject	11.94	0.169	0.18	3.26	50.48	95.4	4.2	192.0
10	hold/start	12.04	0.159	0.17	3.26	50.56	93.5	4.2	192.0
	hold/end	12.46	0.119	0.14	3.28	50.89	85.1	4.2	192.0
	airbreak	12.51	0.119	0.14	3.40	52.69	87.1	50.0	192.0
	vac	14.51	0.002	0.14	0.07	1.05	1.7	1.0	192.0
	airbreak	14.56	0.002	0.06	0.19	2.99	3.8	50.0	192.0
15	vac	16.56	0.000	0.06	0.00	0.06	0.1	1.0	192.0
	airbreak	17.06	0.000	0.00	1.94	30.02	28.9	760.0	192.0

The amount of vapor mixture which should be injected in each make up injection can be determined either by continuously monitoring, directly or indirectly, the hydrogen peroxide vapor concentration and the relative humidity within the chamber, or by predicting the concentration of hydrogen peroxide and water vapors over time and relative humidity.

In either situation, whether the amount injected is measured or predetermined, the amount must be at most, just below the amount that would saturate the vapor mixture and cause condensation. Because the concentration of the incoming hydrogen peroxide vapor is known, the hydrogen peroxide vapor concentration following the injection can be monitored indirectly by calculations based on continuously measuring the pressure, temperature and time into the sterilization hold period. A direct method of monitoring hydrogen peroxide vapor concentration is disclosed in the co-pending application of Arthur L. Cummings entitled "System for Monitoring Sterilant Vapor Concentration" filed simultaneously herewith and incorporated herein by reference. Any other suitable direct method of

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monitoring hydrogen peroxide vapor concentration can be used.

- The saturation limit of the vapors will vary depending on the percent composition of the hydrogen peroxide and water vapor mixture, the temperature and the chamber volume. For purposes of discussing the preferred embodiment, the chamber volume is assumed to be 49.29 liters, the injected vapor mixture is a 30 wt% hydrogen peroxide and water mixture and the temperature is 4°C.
- 10 The graphs in FIGS. 1 through 11 are constructed on the basis of those parameters. Other percent compositions, temperatures and chamber volumes can be used with appropriate modification in the calculations.

- The graph in FIG. 4 illustrates how the optimum sterilization cycle can keep the level of hydrogen peroxide vapor in the chamber far above the standard hydrogen peroxide vapor level observed with a single injection and no make-up injections, but slightly below the maximum allowable level to avoid reaching the saturation limit of the vapor mixture. The maximum allowable level decreases with increasing humidity in accordance with the tabulations in Table I. Table II is provided to help illustrate this fact, as set forth below.
- 15  
20

TABLE II

MAXIMUM HYDROGEN PEROXIDE VAPOR CONCENTRATIONS  
(mg/liter) FROM 30% BY WEIGHT LIQUID SOLUTION  
FLASH VAPORIZED AND MAINTAINED AT VARIOUS TEMPERATURES  
AND RELATIVE HUMIDITIES

5

VAPOR TEMPERATURE (°C)	MAX. H <sub>2</sub> O <sub>2</sub>	VAPOR CONCENTRATION (mg/liter)			
		RELATIVE HUMIDITY			
		0%	20%	40%	80%
10	1	0.389	0.263	0.168	0.041
	2	0.419	0.284	0.180	0.046
	3	0.452	0.307	0.197	0.049
	4	0.487	0.332	0.208	0.052
	5	0.524	0.357	0.228	0.058
	6	0.563	0.385	0.245	0.061
15	7	0.606	0.415	0.264	0.066
	8	0.651	0.444	0.287	0.073
	9	0.699	0.478	0.303	0.078
	10	0.750	0.513	0.325	0.081
20	20	1.48	1.02	0.661	0.166
	30	2.79	1.94	1.26	0.302
	40	5.03	3.54	2.28	0.519
	60	14.6	10.4	6.8	1.4
	80	37.4	26.8	17.5	3.3

25

The graph of FIG. 4 is based on there being a half life of one minute for hydrogen peroxide degradation. The actual rate of hydrogen peroxide degradation is affected by the type of

materials within the chamber and the chamber itself. Some materials catalyze the degradation process and should be avoided or kept to a minimum for best results. In addition, for catalytic surfaces, the greater the surface to volume ratio, the faster the rate of the degradation reaction will be. It is noted that for every gram of hydrogen peroxide which degrades to water and oxygen, 0.53 g water and 0.47 g oxygen are produced. At 4°C 100% relative humidity corresponds to 6.4 mg water vapor per Liter.

The times in FIG. 4 coordinate with times in Table I and FIGS. 1 through 11. Thus, time 4.5 represents the point at which the hydrogen peroxide-water vapor mixture is initially injected into the sterilization chamber. About half a minute later (time = 5.2), a make-up injection of about 0.16 mg/L 30 wt% hydrogen peroxide-water vapor is introduced into the chamber, raising the hydrogen peroxide concentration by about 0.05 mg/L to about .39 mg/L (See Table I). Additional make-up injections are made about every thirty seconds. With each make-up injection and the continuing degradation of the hydrogen peroxide, the relative humidity increases and the maximum allowable hydrogen peroxide level within the chamber decreases, as shown. Momentary increases in the maximum allowable vapor phase hydrogen peroxide level occur with each make-up injection because the incoming 30 wt% mixture enriches the hydrogen peroxide-water vapor ratio. The optimum hydrogen peroxide concentration is maintained by carefully calculated make-up injections. For comparison, the hydrogen peroxide concentration which would be in the chamber if there were no make-up injections is also presented by a curve ("Standard Cycle") on the graph in FIG. 4.

The curve of FIG. 4 representing the maximum allowable hydrogen peroxide vapor concentration which corresponds to varying relative humidities, vapor phase hydrogen peroxide/water vapor ratio and temperatures was calculated using data obtained from Tables III and IV set forth below.



TABLE III

TOTAL VAPOR PRESSURE (mm. Hg) OF HYDROGEN  
PEROXIDE-WATER SOLUTION

5	Temp. (°C)	Mole Fraction Hydrogen Peroxide in Liquid										
		0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0
10	0	4.58	4.06	3.45	2.81	2.20	1.66	1.21	0.856	0.593	0.404	0.272
	10	9.20	8.17	6.96	5.70	4.49	3.42	2.53	1.83	1.30	0.915	0.642
	20	17.5	15.6	13.3	10.9	8.69	6.68	5.00	3.66	2.64	1.89	1.36
	25	23.7	21.1	18.1	14.9	11.9	9.17	6.90	5.09	3.71	2.69	1.95
	30	31.8	28.3	24.3	20.1	16.0	12.4	9.41	6.99	5.14	3.77	2.77
	40	55.3	49.3	42.4	35.2	28.3	22.2	17.0	12.8	9.55	7.14	5.36
	50	92.6	82.5	71.1	59.3	48.1	37.9	29.3	22.4	17.0	12.9	9.90
15	60	149	133	115	96.6	78.7	62.6	49.0	37.8	29.1	22.5	17.5
	70	234	209	181	152	125	100	79.0	61.8	48.2	37.8	20.8
	80	355	318	216	233	192	155	124	97.8	77.2	61.3	49.1
	90	526	471	410	348	289	235	189	150	120	96.5	78.2
	100	760	682	595	507	422	346	280	226	182	148	121
20	110	1074	965	845	722	605	499	407	331	269	221	182
	120	1489	1339	1175	1008	848	704	578	474	389	322	269
	130	2025	1824	1604	1381	1168	974	807	666	552	460	387
	140	2709	2443	2153	1860	1580	1326	1105	919	767	645	546
	150	3568	3222	2847	2467	2105	1776	1489	1247	1048	887	755

\* reprinted from W.C. Schumb, et al. "Hydrogen Peroxide", pp. 221-227  
 25 (Reinhold pub. 1955) based on experimental data from several sources.

TABLE IV  
 VAPOR COMPOSITION (MOLE FRACTION  $H_2O_2$ )<sup>\*</sup> OVER  
 HYDROGEN PEROXIDE-WATER SOLUTIONS

Temp. (°C)	Mole Fraction Hydrogen Peroxide in Liquid								
	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0	0.002	0.006	0.015	0.031	0.060	0.112	0.202	0.352	0.600
10	0.003	0.008	0.018	0.037	0.070	0.128	0.224	0.381	0.626
20	0.003	0.009	0.020	0.041	0.077	0.138	0.238	0.397	0.640
25	0.003	0.010	0.022	0.044	0.081	0.144	0.247	0.407	0.648
30	0.003	0.010	0.023	0.046	0.085	0.151	0.255	0.417	0.656
40	0.004	0.012	0.026	0.052	0.094	0.163	0.272	0.435	0.671
50	0.005	0.014	0.030	0.057	0.103	0.175	0.287	0.452	0.684
60	0.005	0.015	0.033	0.063	0.111	0.187	0.302	0.468	0.696
70	0.006	0.017	0.036	0.068	0.120	0.199	0.316	0.482	0.707
80	0.007	0.019	0.040	0.074	0.128	0.210	0.329	0.495	0.716
90	0.007	0.021	0.043	0.080	0.136	0.221	0.342	0.508	0.725
100	0.008	0.023	0.047	0.085	0.144	0.231	0.354	0.519	0.733
110	0.009	0.025	0.051	0.091	0.152	0.241	0.365	0.530	0.740
120	0.010	0.027	0.054	0.097	0.160	0.251	0.376	0.540	0.747
130	0.011	0.029	0.058	0.102	0.168	0.260	0.386	0.549	0.753
140	0.012	0.031	0.061	0.108	0.175	0.269	0.396	0.558	0.758
150	0.013	0.033	0.065	0.113	0.182	0.278	0.403	0.566	0.763

\* reprinted from W.C. Schumb, et al. "Hydrogen Peroxide", pp. 221-227 (Reinhold pub. 1955) based on experimental data from several sources.

In order to predetermine the optimum hydrogen peroxide vapor concentration for a particular sterilization cycle, a series of complex and interactive calculations must be made. First, the saturation limit of the vapor mixture must be determined. Although the calculations are based on known data it would not be immediately apparent to use the data as described herein because the data of Tables III and IV describe natural conditions whereas the

the corresponding mixtures. The vapor mixture of the present method is a binary mixture which is preferably flash vaporized according to the method described in Bier U.S. Patent No.

4,642,165 the relevant portions of which are hereby incorporated herein by reference. The forced vaporization produces higher concentrations of hydrogen peroxide in the vapor mixture than would be found with natural vaporization from a solution.

In a closed system, a liquid mixture containing  $X_h$  mole fraction hydrogen peroxide and  $X_w$  mole fraction water is in equilibrium with a saturated vapor mixture of  $Y_h$  mole fraction hydrogen peroxide and  $Y_w$  mole fraction water whose concentrations are proportional to partial pressures  $P_h$  and  $P_w$ , respectively. The partial pressures,  $P_h$  and  $P_w$  equal the total pressure,  $P$ . ( $P_h + P_w = P$ ). The vapor composition  $Y_h$  and  $Y_w$  equals one ( $Y_h + Y_w = 1$ ) and the liquid composition,  $X_h$  and  $X_w$  also equals one ( $X_h + X_w = 1$ ). The partial pressure equals the product of the total pressure and the vapor composition ( $P_h = Y_h * P$ ;  $P_w = Y_w * P$ ).

The saturation limit can be determined by measuring vapor concentrations in equilibrium with liquid mixtures. The data in Tables III and IV represents known vapor pressure and vapor composition over liquid mixtures of hydrogen peroxide and water based on measurements of such mixtures gathered from several sources. Vapor concentrations at saturation can be determined for a given temperature by combining vapor composition data from Table IV with vapor pressure data from Table III.

For example, Table IV shows that at 20°C, vapor composed of 0.020 mole fraction hydrogen peroxide ( $Y_h = 0.020$ ,  $Y_w = 0.980$ ) would be in equilibrium with liquid composed of 0.3 mole fraction hydrogen peroxide ( $X_h = 0.3$ ,  $X_w = 0.7$ ). Table III provides that, at 20°C, total vapor pressure ( $P_h + P_w$ ) over 0.3 mole fraction hydrogen peroxide mixture is 10.9 mm Hg. The ideal gas law, ( $PV = nRT$ ) together with the respective molecular weights of the vapors, can be used to calculate the concentrations of the hydrogen peroxide and water vapor

components of the vapor mixture according to the following relationships.

$$C = w/V = Mn/V = MYP/(RT)$$

5 where C = the concentration of vapor, eg., mg/L  
 w = mass  
 V = Volume  
 M = molecular weight  
 n = moles of vapor  
 P = total vapor pressure  
 10 Y = vapor mole fraction  
 R = universal gas constant  
 T = temperature of vapor (and liquid)

In the present example, at 20°C the saturated hydrogen peroxide vapor concentration is determined by the relationship  
 15  $C = MYP/RT$ , or

$$\frac{(34.02 \text{ g/mole}) (0.02) (10.9 \text{ mm Hg})}{(760 \text{ mm Hg/atm}) (0.082 \frac{\text{liter-atm}}{\text{mole} \cdot ^\circ\text{K}}) (293^\circ\text{K})} = 0.00041 \text{ g/L}$$

The saturated water vapor concentration is similarly  
 20 determined.

$$\frac{(18.02 \text{ g/mole}) (0.98) (10.9 \text{ mm Hg})}{(760 \text{ mm Hg/atm}) (0.082 \frac{\text{liter-atm}}{\text{mole} \cdot ^\circ\text{K}}) (293^\circ\text{K})} = 0.0105 \text{ g/L}$$

Thus, at 20°C, in the presence of 10.5 mg/L water vapor,  
 25 the saturation limit for hydrogen peroxide vapor is 0.41 mg/L.  
 This process can be repeated for any combination of temperature  
 and vapor composition by appropriate interpolation between  
 values in Tables III and IV. For example, at 4°C (the  
 temperature of the sterilization method represented in the  
 30 Figures) interpolating from the data in Tables III and IV and  
 using the relationship  $C = MYP/RT$ , in the presence of 1.1 mg/L

water vapor, the saturation limit for hydrogen peroxide vapor is about .5 mg/L, or a 30 wt% (0.185 mole fraction) hydrogen peroxide-water vapor mixture.

Alternatively, the equations, by which the data of the  
5 Tables were calculated, can be used. The equations given by W. C. Schumb, et al. supra at pp. 225-227, are set forth below:

$$P = P_{w_o} * X_w * w + P_{h_o} * (1 - X_w) * h$$

$$Y_h = \frac{P_{h_o} * X_h * h}{P} = \frac{P_{h_o} * X_h * h}{(P_{w_o} * X_w * w) + (P_{h_o} * X_h * h)}$$

- 10 wherein P = total vapor pressure  
 $P_{w_o}$  = vapor pressure of pure water  
 $P_{h_o}$  = vapor pressure of anhydrous hydrogen peroxide  
 $X_{w_o}$  = liquid mole fraction composition of water  
 $X_h$  = liquid mole fraction composition of hydrogen  
 15 peroxide  
 $w$  = activity coefficient for water  
 $h$  = activity coefficient for hydrogen peroxide  
 $Y_h$  = vapor mole fraction composition of hydrogen  
 20 peroxide  
 $*$  = multiplication symbol

Formulas are also given by Schumb et al. supra. for the calculation of  $P_{w_o}$  and  $P_{h_o}$  as functions of temperature, and for the calculation of  $w$  and  $h$  as functions of temperature and liquid composition.

25 In practice, the water vapor concentration, and therefore, the corresponding saturation limit for hydrogen peroxide vapor in the sterilization cycle is not static, but constantly changing due to the degradation of the hydrogen peroxide vapor to water and oxygen. The calculations must be repeated for the  
 30 changing conditions throughout the sterilization stage of the cycle. The calculation process is complex and iterative, when starting from vapor composition, and is best accomplished with the aid of a suitably programmed computer.

The method of the present invention requires knowledge of  
 35 the amount of vapor of one composition that can be added to

vapor of another composition and not exceed the new saturation limit which will result from the additional amount of vapor. The complexity of the situation can be realized if one visualizes incremental addition of the first composition (vapor A, the vapor mixture comprising make-up injection) to the second (vapor B, the vapor mixture within the chamber prior to a particular make-up injection). Each composition has an associated saturation limit. Addition of some of vapor A to vapor B changes the composition of vapor B and a new saturation limit applies. Another increment of vapor A added to vapor B further alters the composition of vapor B and the associated saturation limit.

The calculation of the amount of vapor A that can be added to vapor B to reach, but not exceed, the saturation limit was accomplished by an incremental approach. Compositions of vapor B and saturation limits resulting from incremental additions of vapor A were calculated. If the saturation limit was greater than the concentration in the new vapor B, another increment was calculated. If the saturation limit was exceeded, the calculation was backed up one step, and a smaller incremental addition was calculated. Eventually, the saturation limit on addition of vapor A was determined to the desired precision (0.2%).

Table II shows the results of those calculations for a few specific cases. Vapor A was 30 wt% (0.185 mole fraction) hydrogen peroxide and water vapor mixture ( $Y_h = 0.185$ ,  $Y_w = 0.815$ ). Vapor B initially contained only water vapor, no hydrogen peroxide. Water vapor concentrations head the columns of Table II, and are given as relative humidities (0%, 20%, 40%, 80%). The 0% column is for no water vapor, that is, vapor B is vacant initially. Thus, the 0% column shows the saturation limit of 30 wt% hydrogen peroxide/water vapor. For the

other columns, the initial water vapor concentration varies with temperature.

To calculate the data of Table II, refer again to Table IV to find by interpolation the mole fraction liquid hydrogen peroxide corresponding to 0.185 mole fraction hydrogen peroxide vapor. Then refer to Table III to find the total vapor pressure corresponding to that mole fraction liquid hydrogen peroxide and temperature.

10 The total pressure obtained from Table III is used to calculate the saturated hydrogen peroxide and water vapor concentrations in mg/L according to the relationship  $C = MYP/RT$  as described previously.

For example, and ignoring for the moment the desired temperature conditions, from Table IV, a 0.185 mole fraction hydrogen peroxide vapor corresponds most nearly to 0.6 mole fraction liquid hydrogen peroxide at 60°C, which in turn from Table III, corresponds to 49.0 mm Hg total pressure of the hydrogen peroxide-water mixture.

20 Using the relationship  $C=MYP/RT$ , the concentrations of saturated hydrogen peroxide and water vapors at 0% relative humidity are 14.9 mg/L and 34.7 mg/L, respectively. Table II shows 14.6 mg/L as the saturation limit, rather than 14.9, because of minor differences between the processes of interpolation (used in this example) and iteration on the equations (used to construct Table II).

At 20% relative humidity, there is another source of water vapor in the chamber. When a 30 wt% hydrogen peroxide-water vapor mixture is injected, the new composition will have an actual hydrogen peroxide percentage composition at something less than 30 wt%. The concentration of hydrogen peroxide vapor at the saturation limit is not known however, until it is reached. Therefore, as mentioned above, the

concentration must be increased mathematically by increments to predict what the saturation limit in an actual sterilization cycle would be over time under the desired conditions. The resulting concentrations of saturated hydrogen peroxide and water vapors are 10.4 mg/L and 51.0 mg/L, respectively. The final vapor composition at saturation calculates to be 0.097 mole fraction hydrogen peroxide (0.903 mole fraction water), or 16.9 wt% hydrogen peroxide.

Table I shows results of such calculations for specific cases of a sterilization cycle. All but a few of these cases are more complex than those of Table II. After 4.5 minutes in Table I, Vapor B contains hydrogen peroxide vapor as well as water mixture. Vapor A is still a 30 wt% hydrogen peroxide and water mixture. The hydrogen peroxide and water vapor concentrations of Vapor B continually change due to time-dependent degradation of hydrogen peroxide vapor and injections of vapor A. The saturation limit (column labeled " $\text{H}_2\text{O}_2$  satn, mg/L") change in accordance with changing hydrogen peroxide and water vapor concentrations in Vapor B (" $\text{H}_2\text{O}_2$ , mg/L" and "Water, mg/L," respectively).

After 4.7 minutes in Table I injections of 30 wt% hydrogen peroxide vapor into an essentially vacant chamber at 4° C reached the saturation limit of 0.49 mg vapor phase hydrogen peroxide per Liter. The saturation limit is the same as in Table II for 4° C and 0% relative humidity.

After several periods of decomposition and make-up injections, at 9.86 minutes, the saturation limit is 0.17 mg vapor phase hydrogen peroxide per Liter. The vapor is no longer 30 wt%. Rather, it is only 4.7 wt% hydrogen peroxide (95.3 wt% water), or 0.025 mole fraction hydrogen peroxide. Interpolations of Table IV and of



Table III (or iterative solution of the basic equations) provide the saturation limit of 0.17 mg/L.

The next entry in Table I, "inject" at 9.86 minutes, shows conditions immediately following instantaneous  
5 injection of 8 mg of 30 wt% hydrogen peroxide mixture. Hydrogen peroxide concentration increased by 0.05 mg/L, to 0.176. This is greater than the saturation limit prior to injection, yet the "Vapor % satn" column shows only 86.3% saturated. The saturation limit also  
10 increased, because the hydrogen peroxide mole fraction increased to 0.0333. Table IV indicates that 0.0333 mole fraction hydrogen peroxide at 4° C corresponds to 0.4 mole fraction liquid, which corresponds to 3.11 torr saturation pressure in Table III. This leads, through  
15 use of the relationship  $C = MYP/RT$  described previously, to the saturation limit of 0.20 mg/L hydrogen peroxide shown in Table I.

Figure 4 illustrates the saw-tooth course of both the hydrogen peroxide vapor concentration and the  
20 saturation limit as decomposition periods and make-up injections alternate. Water vapor concentration increases with both decomposition and make-up injections, so as time progresses the saturation limit and the actual hydrogen peroxide vapor concentration get closer  
25 together. The size of further make-up injections would have to decrease to avoid saturation. Eventually, make-up injections could not be made without exceeding the saturation limit.

SUBSTITUTE SHEET

What is claimed is:

1. A sterilization method comprising:  
injecting a hydrogen peroxide and water vapor mixture into a closed sterilization chamber having a predetermined volume at a predetermined temperature in an initial amount approaching the saturation limit of said vapor mixture in said chamber at said temperature and said volume; and,

thereafter, injecting a plurality of intermittent make-up injections of said vapor mixture into said chamber, said make-up injections being at a rate and each said make-up injection being in a variable amount necessary to maintain the concentration of hydrogen peroxide vapor at a level effective for sterilization but less than that concentration of hydrogen peroxide vapor which would raise the concentration of said vapor mixture to the saturation limit which will be present in said chamber immediately following injection of such make-up injection at said temperature.

2. The method of claim 1 wherein said hydrogen peroxide and water vapor mixture has a percent composition of 30% by weight.

3. The method of claim 1 wherein said temperature is about 4°C.

4. The method of claim 1 wherein said initial amount, each said variable amount and the saturation limits for said vapor mixture are predetermined.

5. The method of claim 1 where in the saturation limits for said vapor mixture and each said variable amount are determined by continuously monitoring the relative humidity and the hydrogen peroxide vapor concentration within said chamber.

**SUBSTITUTE SHEET**

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Fig. 1.

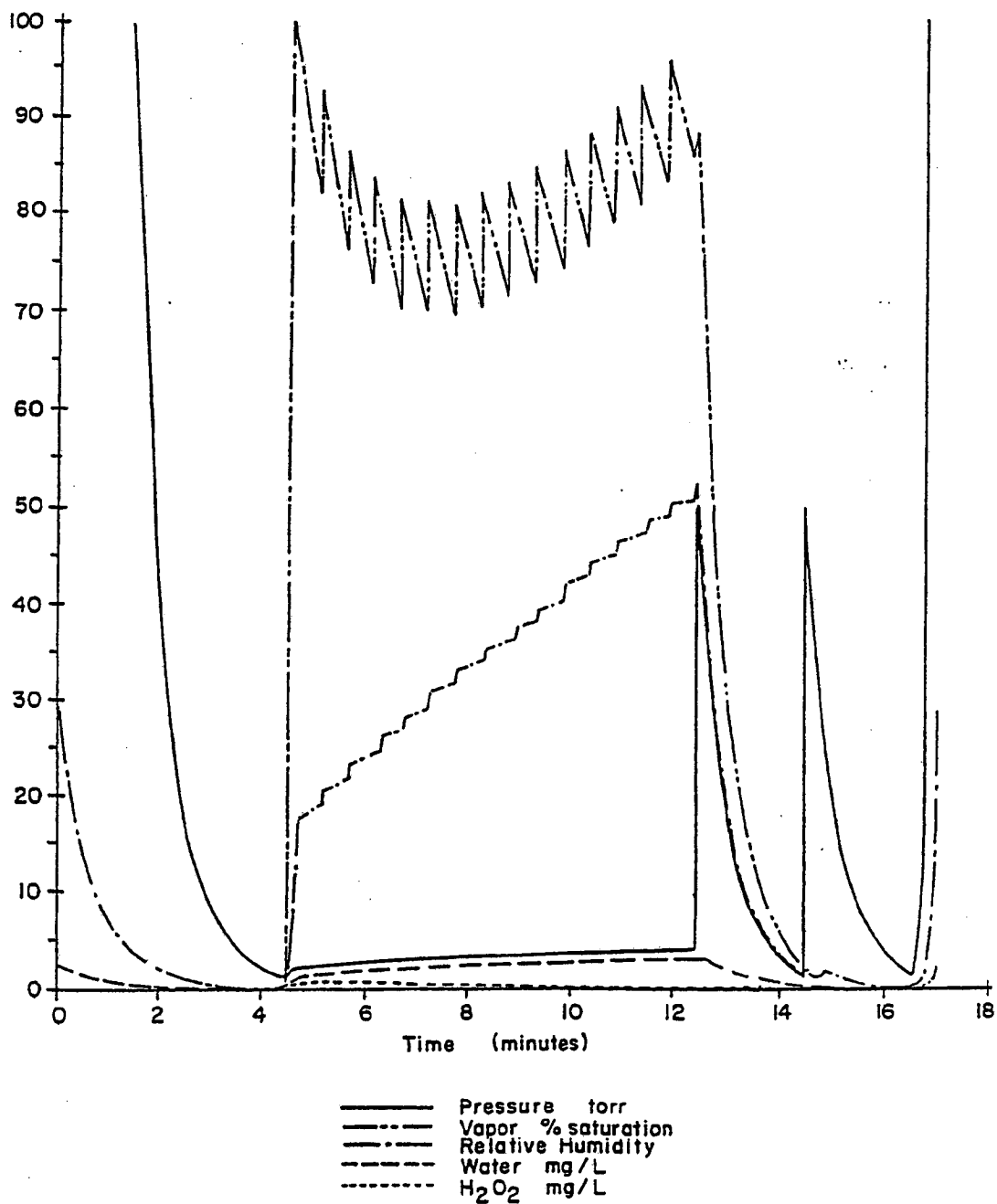


Fig. 2.

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Simulation of  $H_2O_2$  Cycle  
in 49.29L chamber at 4°C

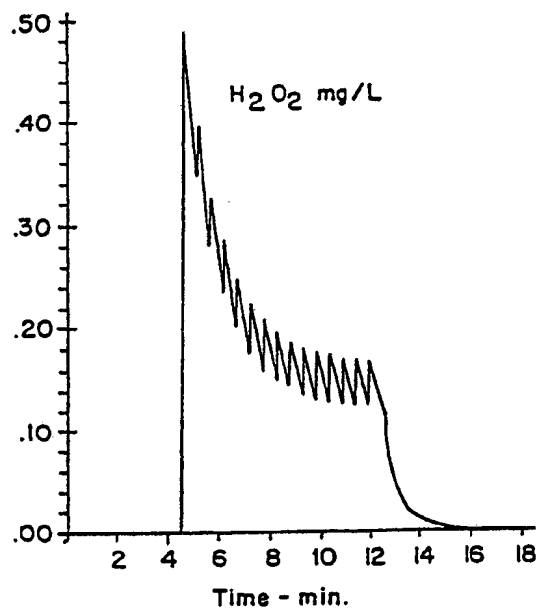


Fig. 3.

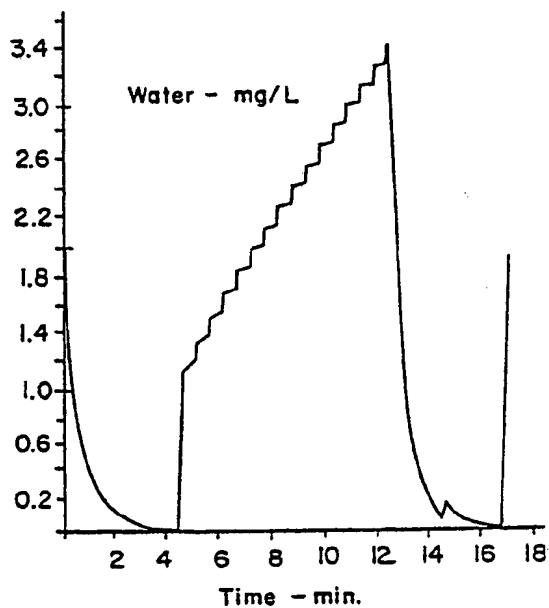


Fig. 6.

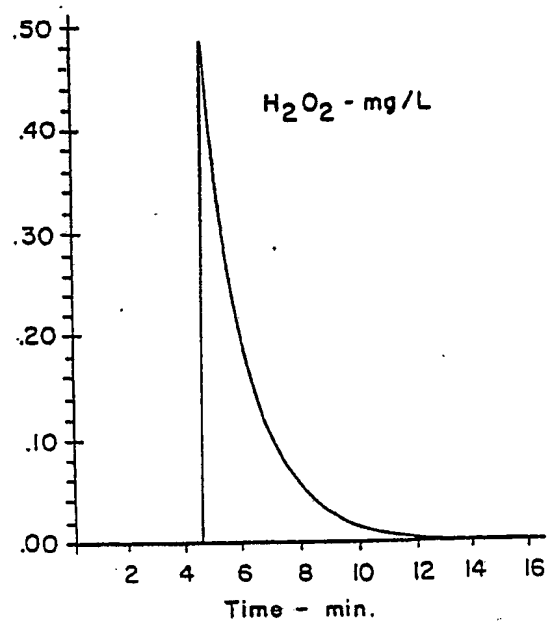
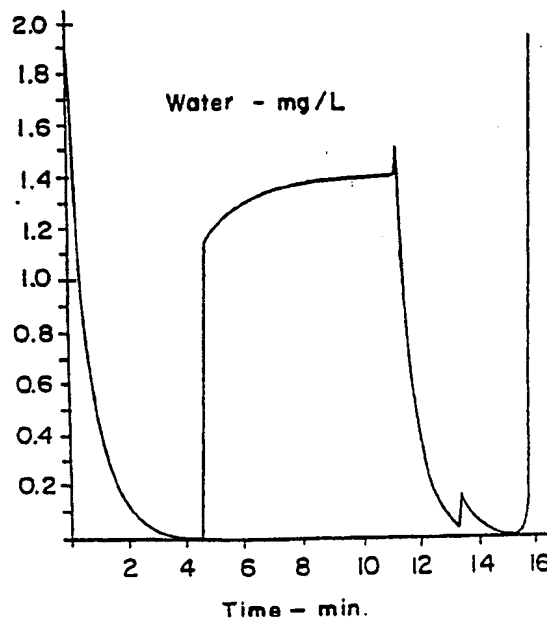
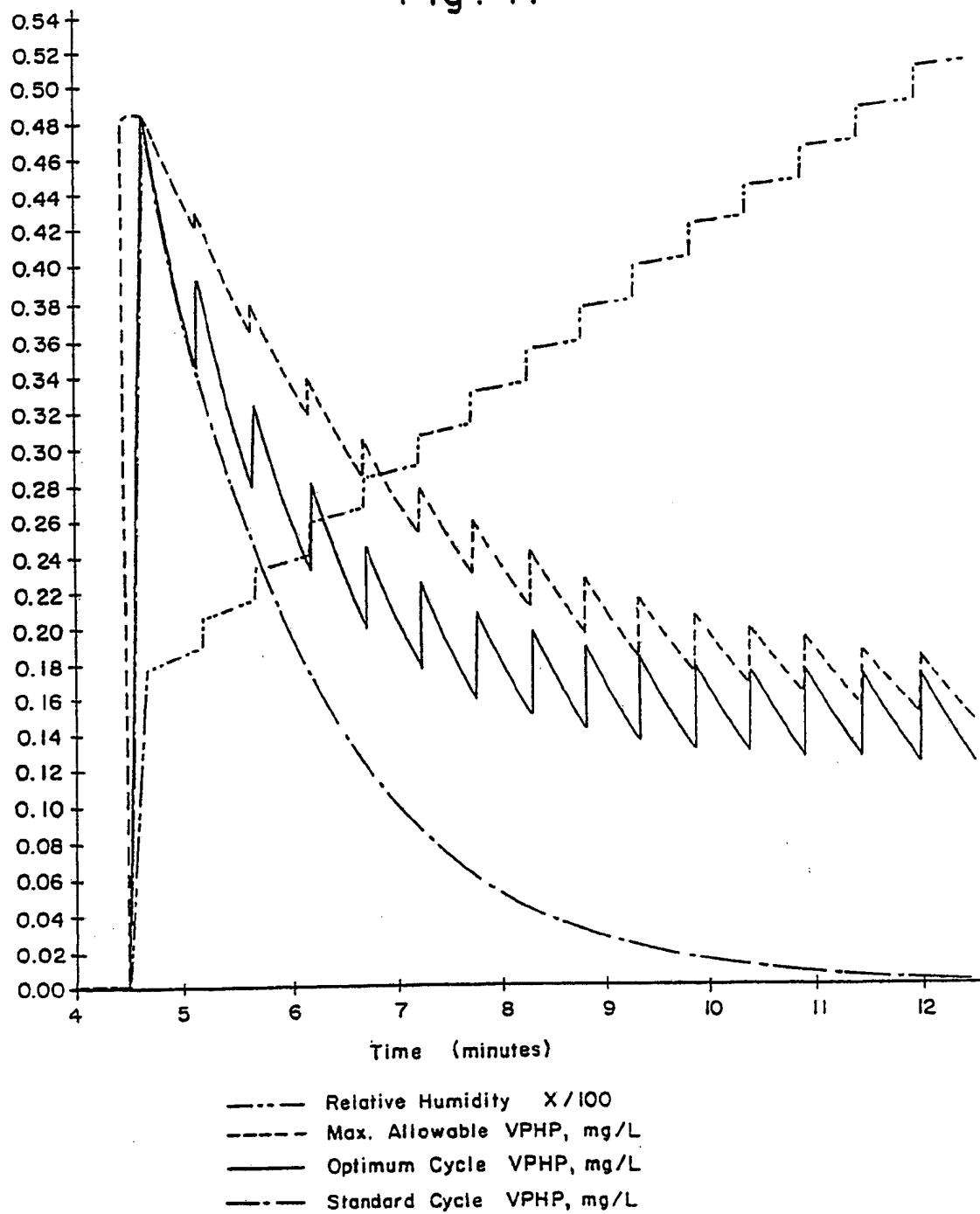


Fig. 7.



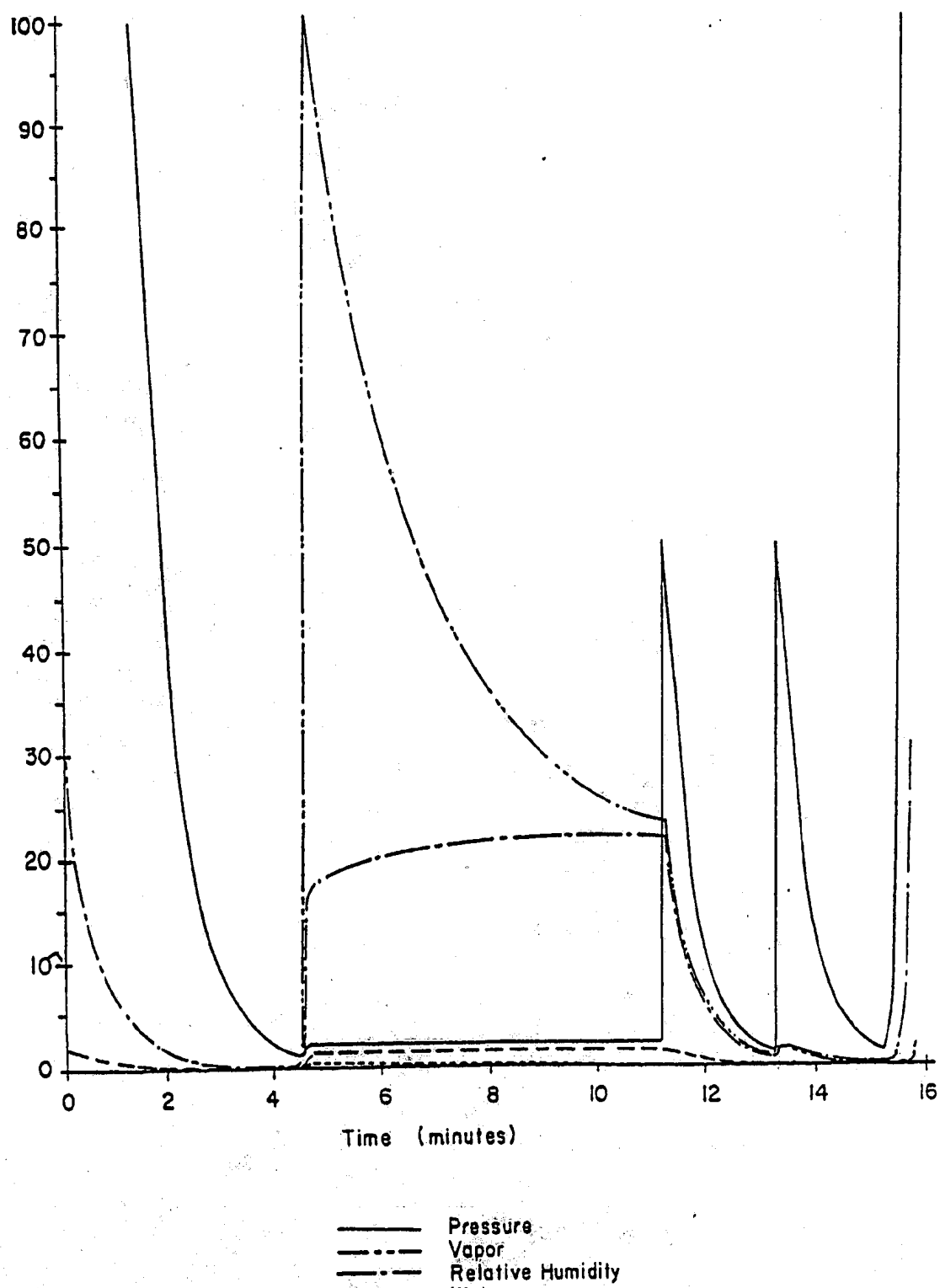
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Fig. 4.



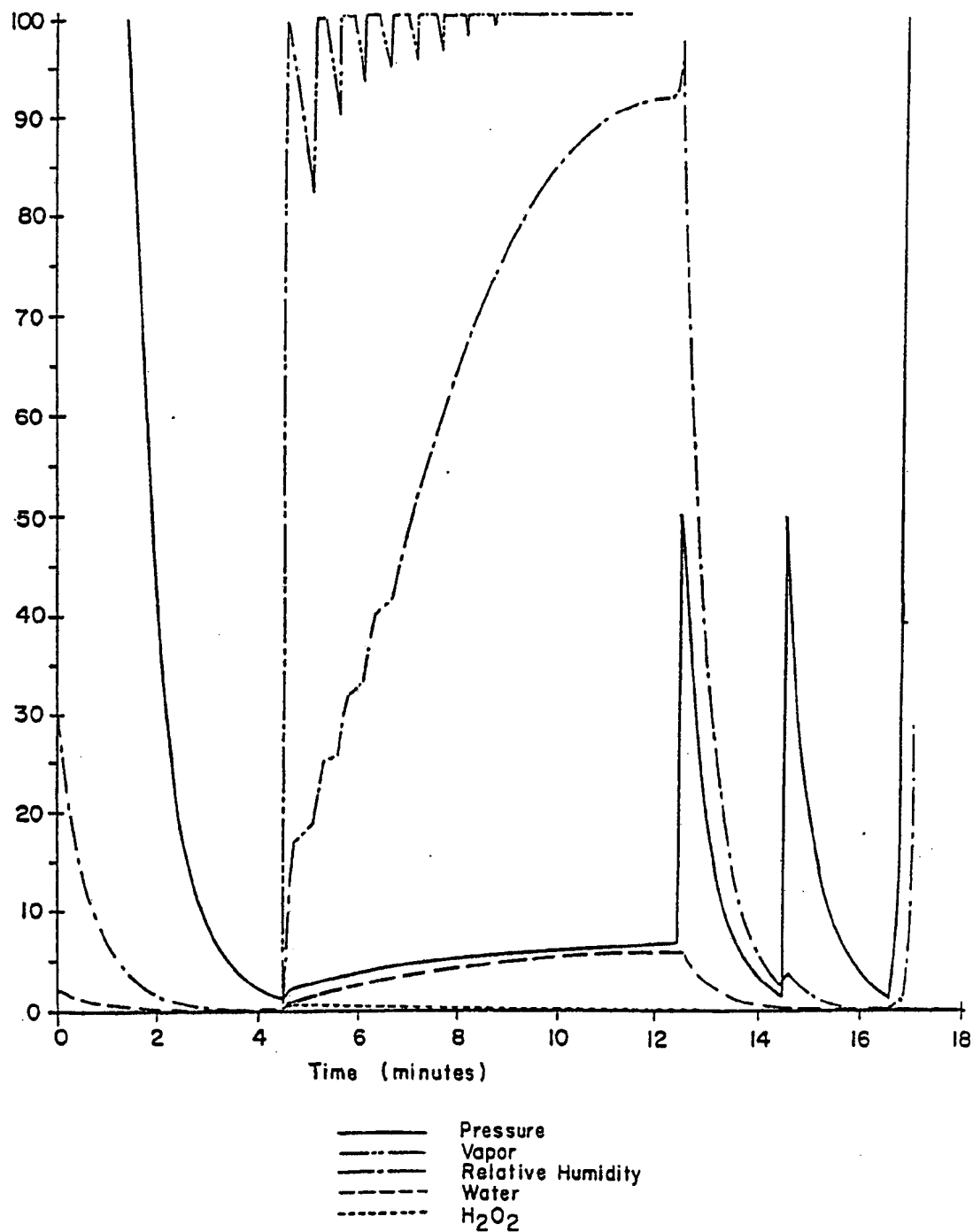
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Fig.5.



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Fig. 8.





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Fig. 9.

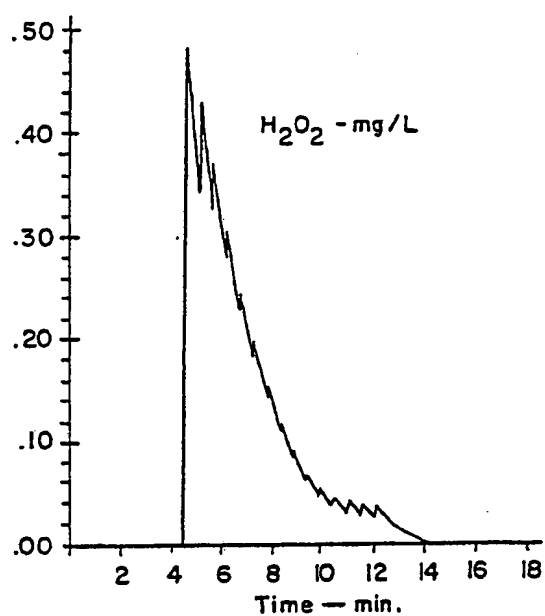


Fig. 10.

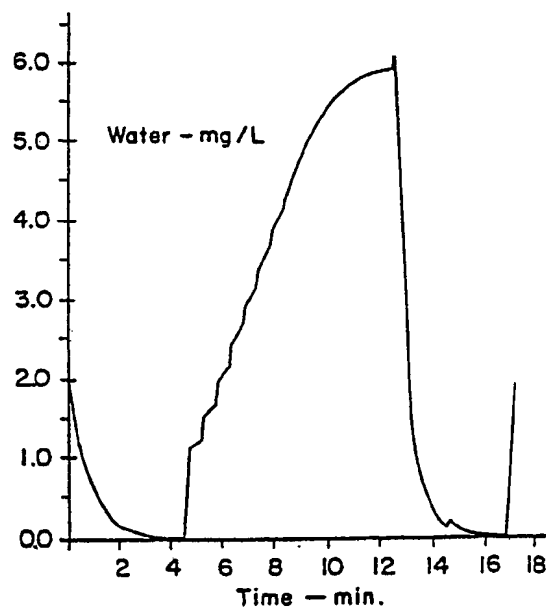
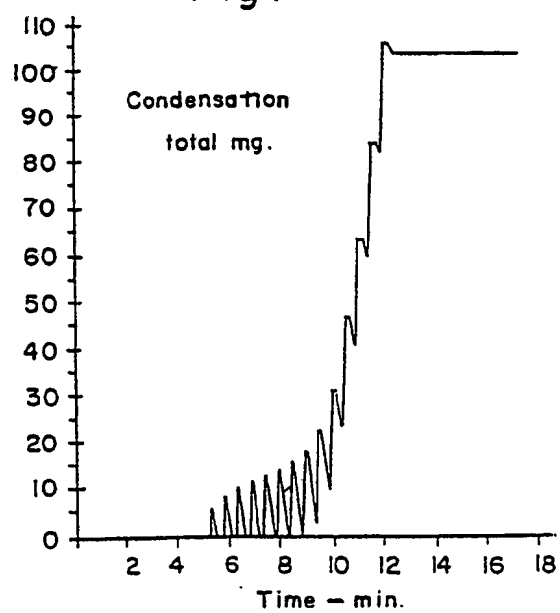


Fig. 11.



# INTERNATIONAL SEARCH REPORT

International Application No PCT/US 88/04508

<b>I. CLASSIFICATION OF SUBJECT MATTER</b> (If several classification symbols apply, indicate all) <sup>6</sup> According to International Patent Classification (IPC) or to both National Classification and IPC <b>IPC4: A 61 L 2/20</b>																	
<b>II. FIELDS SEARCHED</b> <div style="text-align: right; font-size: small;">Minimum Documentation Searched <sup>7</sup></div> <table style="width: 100%; border: none;"> <tr> <td style="width: 20%; border: none;">Classification System <sup>1</sup></td> <td style="border: none;">Classification Symbols</td> </tr> <tr> <td style="border: none; height: 40px; vertical-align: bottom;">IPC4</td> <td style="border: none; height: 40px; vertical-align: bottom;">A 61 L</td> </tr> </table> <div style="text-align: center; font-size: x-small; margin-top: 5px;">             Documentation Searched other than Minimum Documentation              to the extent that such Documents are included in the Fields Searched <sup>8</sup> </div>			Classification System <sup>1</sup>	Classification Symbols	IPC4	A 61 L											
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IPC4	A 61 L																
<b>III. DOCUMENTS CONSIDERED TO BE RELEVANT <sup>9</sup></b> <table border="1" style="width: 100%; border-collapse: collapse; font-size: small;"> <thead> <tr> <th style="width: 10%;">Category <sup>10</sup></th> <th style="width: 60%;">Citation of Document, <sup>11</sup> with indication, where appropriate, of the relevant passages <sup>12</sup></th> <th style="width: 30%;">Relevant to Claim No. <sup>13</sup></th> </tr> </thead> <tbody> <tr> <td style="text-align: center; vertical-align: top;">A</td> <td>US, A, 4642165 (MARK E. BIER) 10 February 1987, see the whole document --</td> <td style="text-align: center; vertical-align: top;">1-5</td> </tr> <tr> <td style="text-align: center; vertical-align: top;">A</td> <td>US, A, 4169123 (FRANCIS C. MOORE ET AL) 25 September 1979, see the whole document --</td> <td style="text-align: center; vertical-align: top;">1-5</td> </tr> <tr> <td style="text-align: center; vertical-align: top;">A</td> <td>WO, A1, 88/04939 (AMERICAN STERILIZER COMPANY) 14 July 1988, see the whole document --</td> <td style="text-align: center; vertical-align: top;">1-5</td> </tr> <tr> <td style="text-align: center; vertical-align: top;">P,A</td> <td>US, A, 4744951 (ARTHUR L. CUMMINGS ET AL) 17 May 1988, see the whole document --</td> <td style="text-align: center; vertical-align: top;">1-5</td> </tr> </tbody> </table>			Category <sup>10</sup>	Citation of Document, <sup>11</sup> with indication, where appropriate, of the relevant passages <sup>12</sup>	Relevant to Claim No. <sup>13</sup>	A	US, A, 4642165 (MARK E. BIER) 10 February 1987, see the whole document --	1-5	A	US, A, 4169123 (FRANCIS C. MOORE ET AL) 25 September 1979, see the whole document --	1-5	A	WO, A1, 88/04939 (AMERICAN STERILIZER COMPANY) 14 July 1988, see the whole document --	1-5	P,A	US, A, 4744951 (ARTHUR L. CUMMINGS ET AL) 17 May 1988, see the whole document --	1-5
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P,A	US, A, 4744951 (ARTHUR L. CUMMINGS ET AL) 17 May 1988, see the whole document --	1-5															
<div style="display: flex; justify-content: space-between; font-size: x-small;"> <div style="width: 45%;"> <p>• Special categories of cited documents: <sup>14</sup></p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier document but published on or after the international filing date</p> <p>"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> </div> <div style="width: 45%;"> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step</p> <p>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.</p> <p>"G" document member of the same patent family</p> </div> </div>																	
<b>IV. CERTIFICATION</b> Date of the Actual Completion of the International Search <b>28th March 1989</b>		Date of Mailing of this International Search Report <b>19. 04. 89</b>															
International Searching Authority <b>EUROPEAN PATENT OFFICE</b>		Signature of Authorized Officer <b>P.C.G. VAN DER PUTTEN</b>															

## III. DOCUMENTS CONSIDERED TO BE RELEVANT (CONTINUED FROM THE SECOND SHEET)

Category *	Citation of Document, with indication, where appropriate, of the relevant passages	Relevant to Claim No
A	EP, A2, 0177123 (AMERICAN STERILIZER COMPANY) 9 April 1986, see the whole document -- -----	1-5

ANNEX TO THE INTERNATIONAL SEARCH REPORT  
ON INTERNATIONAL PATENT APPLICATION NO.

PCT/US 88/04508

SA

26248

This annex lists the patent family members relating to the patent documents cited in the above-mentioned international search report.  
The members are as contained in the European Patent Office (EPO) file on 12/01/89  
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Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US-A- 4642165	10/02/87	NONE	
US-A- 4169123	25/09/79	NONE	
WO-A1- 88/04939	14/07/88	EP-A- 0294418	14/12/88
US-A- 4744951	17/05/88	AU-D- 35150/84 DE-A- 3440714	16/05/85 13/06/85
EP-A2- 0177123	09/04/86	US-A- 4687635	18/08/87

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